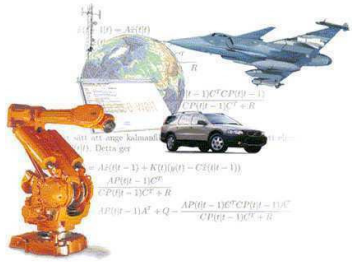


Linear Systems

Lecture 3. Controllability

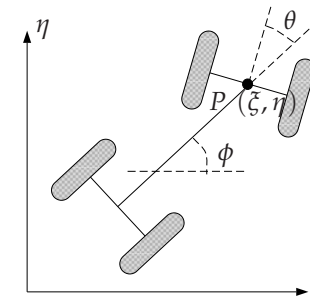


Torkel Glad

Reglerteknik, ISY, Linköpings Universitet

Controllability. Example

Motion planning for a vehicle:



u_1 : turning speed of front wheels, u_2 : forward speed

$$\dot{\theta} = u_1, \quad \dot{\phi} = u_2 \sin \theta$$

$$\dot{\xi} = u_2 \cos(\theta + \phi), \quad \dot{\eta} = u_2 \sin(\theta + \phi)$$

Example, cont'd

In vector form

$$\frac{d}{dt} \begin{bmatrix} \theta \\ \phi \\ \xi \\ \eta \end{bmatrix} = u_1 \underbrace{\begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix}}_{f_1} + u_2 \underbrace{\begin{bmatrix} 0 \\ \sin \theta \\ \cos(\theta + \phi) \\ \sin(\theta + \phi) \end{bmatrix}}_{f_2}$$

How can you span a 4-dimensional space with 2 vectors?

The differential equation solution

$$\dot{x} = f(x)$$

Taylor expansion:

$$x(h) = x(0) + h\dot{x}(0) + \frac{h^2}{2}\ddot{x}(0) + O(h^3)$$

Using $\dot{x} = f$, $\ddot{x} = f_x f$

$$x(h) = x(0) + hf(x(0)) + \frac{h^2}{2}(f_x f)(x(0)) + O(h^3)$$

Expanding about $x_o = x(0) + O(h)$

$$x(h) = x(0) + h(f(x_o) + f_x(x_o)(x(0) - x_o)) + \frac{h^2}{2}(f_{xx})(x_o) + O(h^3)$$

New directions from Lie brackets

- Start at $x = x_0$.
- Solve $\dot{x} = f_1(x)$ for $t \in [0, h]$, then $\dot{x} = f_2(x)$ for $t \in [h, 2h]$, then $\dot{x} = -f_1(x)$ for $t \in [2h, 3h]$, then $\dot{x} = -f_2(x)$ for $t \in [3h, 4h]$.
- The resulting movement is $h^2[f_1, f_2](x_0) + O(h^3)$
 - $[f_1, f_2] = f_{2,x}f_1 - f_{1,x}f_2$ is the **Lie bracket**.
- By doing nested movements one can generate $[f_3, [f_1, f_2]]$, $[[f_1, f_2], [f_3, f_4]]$,
- If the set of all possible Lie brackets spans the space, then intuitively one should have full controllability.

Lie brackets for car example

$$[f_1, f_2] = \begin{bmatrix} 0 \\ \cos \theta \\ -\sin(\theta + \phi) \\ \cos(\theta + \phi) \end{bmatrix}, \quad [f_2, [f_1, f_2]] = \begin{bmatrix} 0 \\ 0 \\ \sin(\phi) \\ -\cos(\phi) \end{bmatrix},$$

Evaluation at $x_0 = 0$:

$$f_1 = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix}, \quad f_2 = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \end{bmatrix}, \quad [f_1, f_2] = \begin{bmatrix} 0 \\ 1 \\ 0 \\ 1 \end{bmatrix}, \quad [f_2, [f_1, f_2]] = \begin{bmatrix} 0 \\ 0 \\ 0 \\ -1 \end{bmatrix}$$

Properties of Lie bracket

$$[f, g] = g_x f - f_x g$$

Some Lie bracket formulas:

$$[a, a] = 0$$

$$[a, b] = -[b, a]$$

$$[a + b, c] = [a, c] + [b, c]$$

$$[a, [b, c]] + [b, [c, a]] + [c, [a, b]] = 0 \quad \text{Jacobi identity}$$

Controllability, definitions

- $A_U(x_0)$: the *reachable set* from x_0 , while remaining in the set U
- The system *controllable*: $A_{R^n}(x) = R^n$ for any x .

Problem: If U is a small neighborhood A_U is often “one-sided”

Often the case for systems with drift term:

$$\dot{x} = f(x) + u_1 g_1(x) + \dots + u_m g_m(x)$$

The natural local property is local accessibility:

- The system *locally accessible* at x :
 - $A_U(x)$ has a nonempty interior for any neighborhood U of x
 - i.e. $A_U(x)$ has full dimension.

Controllability, the test:

$$\dot{x} = f(x, u)$$

1. form $f_j(x) = f(x, u_j)$, for all possible constant u_j
2. form all possible linear combinations of all possible iterated Lie brackets of the f_j
3. Hermann and Krener 1977: If they span the state space at x_0 (controllability rank condition), then the system is locally accessible at x_0 .

Controllability, linear systems

$$\dot{x} = Ax + Bu$$

- $[Ax, b_i] = -Ab_i$, where b_i is a column of B
- $[B, AB, \dots, A^{n-1}B]$ full rank \Rightarrow controllability rank condition satisfied.

The linear structure permits much stronger conclusions.

To reach with minimum energy

Control from x_0 to x_f with minimum energy:

$$\dot{x}(t) = A(t)x(t) + B(t)u(t), \quad x(t_0) = x_0, \quad x(t_f) = x_f$$

$$\text{minimize } J = \frac{1}{2} \int_{t_0}^{t_1} u^T u dt$$

The control then has the form

$$u(t) = -B^T(t)\Phi^T(t_0, t)W(t_0, t_1)^{-1}z, \quad z = x_0 - \Phi(t_0, t_1)x_f$$

where W is the *controllability Gramian*

$$W(t_0, t_1) = \int_{t_0}^{t_1} \Phi(t_0, t)B(t)B^T(t)\Phi^T(t_0, t) dt$$

Controllability

The *controllability Gramian*

$$W(t_0, t_1) = \int_{t_0}^{t_1} \Phi(t_0, t)B(t)B^T(t)\Phi^T(t_0, t) dt$$

Theorem Possible to move the state from x_0 at $t = t_0$ to x_1 at $t = t_1$

\Leftrightarrow

$z = x_0 - \Phi(t_0, t_1)x_1$ is in the range space of $W(t_0, t_1)$.

The energy required is

$$J = \frac{1}{2}z^T W(t_0, t_1)^{-1}z$$

Controllability, time invariant case

Time-invariant case (A, B constant):

$$\mathcal{C} = (B \quad AB \quad \dots \quad A^{n-1}B)$$

Theorem The range and null spaces of $W(t_0, t)$ coincide with the range and null spaces of $\mathcal{C}\mathcal{C}^T$ for all $t > t_0$.

Discrete time, time invariant case

$R(t_0, t_1)$ attains maximum rank after at most n time steps (Cayley-Hamilton). The controllability properties are thus given by

$$\mathcal{C} = (B \quad AB \quad \dots \quad A^{n-1}B) = R(t_0, t_0+n)$$

Controllability theory for time invariant systems is thus the same in continuous and discrete time (\dot{x} replaced by $x(t+1)$).

Discrete time

Iterating the state equation gives

$$R(t_0, t_1)U = z$$

where

$$\begin{aligned} U &= [u^T(t_{1-1}) \quad \dots \quad u^T(t_0)]^T \\ z &= x(t_1) - A(t_{1-1}) \dots A(t_0)x(t_0) \\ R(t_0, t_1) &= [B(t_{1-1}) \quad A(t_{1-1})B(t_{1-2}) \quad \dots \\ &\quad \dots \quad A(t_{1-1}) \dots A(t_0+1)B(t_0)] \end{aligned}$$

It is possible to move from $x(t_0)$ to $x(t_1)$ in the time interval $[t_0, t_1]$ if and only if z is in the range space of $R(t_0, t_1)$.

The minimum value of $U^T U$ is $z^T (RR^T)^{-1} z$. RR^T thus corresponds to the continuous time controllability Gramian.

Change of state variables

$$\dot{x} = Ax + Bu, \quad y = Cx, \quad x = T\bar{x}, \quad T \text{ nonsingular}$$

gives

$$\begin{aligned} \dot{\bar{x}} &= \bar{A}\bar{x} + \bar{B}u, \quad y = \bar{C}\bar{x} \\ \bar{A} &= T^{-1}AT, \quad \bar{B} = T^{-1}B, \quad \bar{C} = CT, \quad \bar{e} = T^{-1}e \end{aligned}$$

Controllability is thus preserved under this *similarity transformation*.

Theorem Let the rank of \mathcal{C} be r . Then T can be chosen so that

$$\bar{A} = \begin{pmatrix} \bar{A}_{11} & \bar{A}_{12} \\ 0 & \bar{A}_{22} \end{pmatrix}, \quad \bar{B} = \begin{pmatrix} \bar{B}_{11} \\ 0 \end{pmatrix}$$

where \bar{A}_{11} is $r \times r$, \bar{B}_{11} is $r \times m$ and $\bar{A}_{11}, \bar{B}_{11}$ controllable.

Note: The partition of eigenvalues between \bar{A}_{11} and \bar{A}_{22} is unique: “controllable” and “uncontrollable” eigenvalues

The Kalman decomposition theorem

R range space of controllability matrix; N null space of observability matrix

$$T = [T_1 \quad T_2 \quad T_3 \quad T_4]$$

where T_2 basis for $R \cap N$, $[T_2, T_4]$ basis for N , $[T_1, T_2]$ basis for R .

Then

$$\dot{z} = \begin{bmatrix} \tilde{A}_{11} & 0 & \tilde{A}_{13} & 0 \\ \tilde{A}_{21} & \tilde{A}_{22} & \tilde{A}_{23} & \tilde{A}_{24} \\ 0 & 0 & \tilde{A}_{33} & 0 \\ 0 & 0 & \tilde{A}_{43} & \tilde{A}_{44} \end{bmatrix} z + \begin{bmatrix} \tilde{B}_1 \\ \tilde{B}_2 \\ 0 \\ 0 \end{bmatrix} u$$
$$y = [\tilde{C}_1 \quad 0 \quad \tilde{C}_3 \quad 0]$$

i.e. system decomposed into controllable-observable, controllable-unobservable, uncontrollable-observable and uncontrollable-unobservable parts.

PBH tests

Theorem A, B controllable if and only if

$$p^T A = \lambda p^T, \quad p^T B = 0 \Rightarrow p = 0$$

Theorem A, B controllable if and only if

$$\text{rank}(sI - A \quad B) = n$$

for all complex s .

Nonlinear stabilizability

$$\dot{x} = f(x, u), \quad f(x_0, u_0) = 0$$

Is it possible to find a feedback that gives asymptotic stability at x_0 ?

- Linearization around x_0, u_0 has all “uncontrollable” eigenvalues strictly in left half plane \Rightarrow possible.
- Linearization around x_0, u_0 has an “uncontrollable” eigenvalue strictly in right half plane \Rightarrow impossible.
- Difficult case: “uncontrollable” eigenvalues on imaginary axis.